



www.cerfacs.fr

CENTRE EUROPÉEN DE RECHERCHE ET DE FORMATION AVANCÉE EN CALCUL SCIENTIFIQUE

The behavior of the electron cyclotron drift instability (ECDI) inside Hall Effect Thruster with a fluid code

V. Joncquieres^(1,2), O. Vermorel⁽¹⁾, **B. Cuenot⁽¹⁾**

ExB Workshop - Princeton Plasma Physics Laboratory

1 November 2018

1)CERFACS, Toulouse FRANCE 2) SAFRAN Aircraft Engines, Vernon, FRANCE

Hall effect thrusters: the industrial point of view

SAFRAN industrializes a complete range of plasma Hall effect thrusters for low power electric propulsion:



The PPS-1350 Hall thruster (SAFRAN)



The PPS-5000 Hall thruster (SAFRAN)



Long and costly qualifications in vacuum test facilities

 Until now, no industrial numerical solver is mature enough to help them in the conception and understanding of Hall effect thrusters



The big complexity of Hall effect thruster plasma flows

- <u>Complex plasma phenomena</u> are highlighted through experiments ...
- ... or through simplified numerical problems ...



2D structure of the fluctuating azimuthal component of the electric field in a Hall thruster⁽¹⁾



Rotating spoke instabilities of plasma density on a 6 <u>kW Hall Thruster⁽²⁾</u>



 ... but are still not fully understood. They can decrease thruster efficiency and cause an <u>anormal erosion of</u> <u>ceramics</u> Ageing of the PPS-1350 Hall thruster (SAFRAN)



A numerical solver to model Hall-Effect thruster's flows

<u>Objectives</u>: Develop a **3D unstructured massively parallel** PIC/fluid solver to model with accuracy the plasma behavior inside a Hall Effect Thruster (HET) in collaboration with SAFRAN : <u>AVIP</u>



AVIP-Fluid: Equations

• Fluid equation system for ions and electrons based on a 10-moment model :

$$\begin{split} \partial_t n_e + \nabla .(n_e \vec{u_e}) &= n_e n_n K_{ioniz} \ , \ \partial_t n_i + \nabla .(n_i \vec{u_i}) = n_e n_n K_{ioniz} \\ \partial_t (m_e n_e \vec{u_e}) + \nabla .(m_e n_e \vec{u_e} \vec{u_e} + k_B T_e n_e \overline{\vec{I}}) &= -en_e (\vec{E} + \vec{u_e} \times \vec{B}) - K_{en} n_n n_e m_e (\vec{u_e} - \vec{u_n}) \\ \partial_t (m_i n_i \vec{u_i}) + \nabla .(m_i n_i \vec{u_i} \vec{u_i} + k_B T_i n_i \overline{\vec{I}}) &= en_i (\vec{E} + \vec{u_i} \times \vec{B}) + K_{in} n_n n_i m_i (\vec{u_i} - \vec{u_n}) \\ \partial_t (m_e n_e E_e) + \nabla .\left(\left(\frac{1}{2} m_e n_e \vec{u_e}^2 + \frac{\gamma}{\gamma - 1} P_e\right) . \vec{u_e} + \vec{Q_e} \right) &= -en_e \vec{E} . \vec{u_e} \ -S_{ioniz,e}^2 - S_{exc,e}^2 - S_{en,e}^2 \\ \partial_t (m_i n_i E_i) \ + \nabla .\left(\left(\frac{1}{2} m_i n_i \vec{u_i}^2 + \frac{\gamma}{\gamma - 1} P_i\right) . \vec{u_i} \right) \ &= en_i \vec{E} . \vec{u_i} \ +S_{ioniz,i}^2 - S_{in,i}^2 \end{split}$$

with :

ECERFACS

• $q_{\alpha}n_{\alpha}(\vec{E} + \vec{u_{\alpha}} \times \vec{B})$ the Lorentz force with \vec{E} and \vec{B} the electromagnetic fields, \vec{B} is supposed constant, a Poisson equation solves the variation of the electric potential: $\Delta \phi = \frac{e}{\epsilon_0}(n_i - n_e)$

$$\vec{Q_e}$$
 the electron heat flux is first neglected:

$$\vec{Q}_e = 0$$

• A mass continuity equation for neutrals at constant speed:

$$\partial_t n_n + \nabla (n_n V_{0,n}) = - n_e n_n K_{ioniz}$$

 Extracted from a z-*θ* collisionless PIC simulation with given ionization rate ¹⁾





$$J = e \int_0^d S(x) dx = 400 \text{ A/m}^2$$



<u>Goal : Study this test case with our fluid formulation and observe if the ECDI is triggered by</u> fluid equations

<u>A simplified fluid model :</u>

$$\begin{aligned} \partial_t n_e + \nabla .(n_e u_e) &= S , \quad \partial_t n_i + \nabla .(n_i u_i) = S \\ \partial_t (m_e n_e V_e) + \nabla .(m_e n_e V_e V_e + k_B T_e n_e I) &= -en_e (E + V_e \times B) \\ \partial_t (m_i n_i V_i) + \nabla .(m_i n_i V_i V_i + k_B T_i n_i I) &= en_i (E + V_i \times B) \\ \partial_t (m_e n_e E_e) + \nabla .\left(\left(\frac{1}{2}m_e n_e V_e^2 + \frac{\gamma}{\gamma - 1}P_e\right) .V_e \right) = -en_e E .V_e + \Theta_e \\ \partial_t (m_i n_i E_i) + \nabla .\left(\left(\frac{1}{2}m_i n_i V_i^2 + \frac{\gamma}{\gamma - 1}P_i\right) .V_i \right) = en_i E .V_i + \Theta_i \end{aligned}$$

How to express energy source terms ?

• An ion is created at T_i = 0.5 eV

$$\Theta_i = Sk_BT_i$$

An electron is created at
$$T_e = 10 \text{ eV}$$

$$\Theta_e = Sk_B T_e$$



Simulation 1 with a 500x200 mesh (1 cell per λ_D) and a second order scheme (HLLC-MUSCL) :





The plasma density is too high in the ionization region

E CERFACS

- The bad discretisation of the sheath creates a high electron temperature which pollutes the entire domain
- The sum of ion currents oscillates around the value of ionization current

$$\Gamma_{i,c} + \Gamma_{i,a} = e \int_0^d S(x) dx = 400 \text{ A/m}^2$$



<u>Comparison of the sum of the ion current through</u> electrodes vs creation of ions by ionization





The 12th mode seems to correspond to the good frequency and is one of the highest mode

Investigate this particular mode using a Domain Decomposition Method

ECERFACS

Simulation 1 with a 500x200 mesh (1 cell per λ_D) and a second order scheme (HLLC-MUSCL) :





Conclusions

- An instability appears in the azimuthal direction which has same properties as the Electron Cyclotron Drift Instability
- The fluid simulation fails to reach a steady state, possibly due to the cathode injection model

 Note that a second order numerical scheme is mandatory for a good resolution of electrode sheaths¹⁾